

Efficiency of Sound Radiation from Vibrating Bodies

I. VIBRATION EFFICIENCY

Sound waves are primarily created by the vibration of physical bodies in contact with the air. The motion of the body causes the air in the immediate vicinity of the body to also move. The question I will address here is how much of that motion of the air in the immediate vicinity of the body actually makes it out as sound waves far away from the body, and what is the distribution of the sound energy in direction far away from the vibrating body?

We will look at a number of cases, typified by a loudspeaker enclosed in a wall or in a sound-tight box, a speaker not enclosed, in which sound can reach the listener from both sides of the vibrating cone of the speaker, and sound emitted by a tuning fork, in which one has two vibrating sources, for both of which the sound can get to the listener from both sides of each of the tines of the fork, and in which the two tines are vibrating in opposite directions at all times.

In each of these cases there are two regimes, the one where the wavelength of the sound waves produced by the vibrating body is much larger than the dimensions of the vibrating body, and the other where the dimensions of the body are larger than the wavelength of the sound that is emitted. For musical instruments, the former is almost always (except for the highest frequencies of sound emitted by an instrument) the case. The wavelength of sound at 1kHz (near C two octaves above middle C) is 33 cm, and this is the maximum size of the radiating area of most musical instruments which play notes that high.

Let us characterize the source of the sound by the velocity v of vibration. If the vibration is of the simple harmonic type, (ie, looks like a sin wave if we graph the velocity as a function of time) let us take v as the maximum velocity of the surface vibrating. The energy density in the vibrating air near the piston I will then take to be $\frac{1}{2}\rho v^2$ where ρ is the density of air.

The density is a constant (about $1.2Kg/m^3$) so the important feature of this energy density is that it depends on the square of the velocity of the vibrating object. If all of this energy were carried away from the surface in the escaping sound wave, then the total energy flow away from the surface would be given by the energy density ($\frac{1}{2}\rho v^2$) times the area of the vibrating surface (A) times the velocity of sound (c). This last term is there because after a second the sound energy that was produced at the beginning of the second would be a distance c away at the end of that second. Thus the energy density would be spread over a distance of c away from the speaker. The term A is there because each portion of the area of the vibrating surface produces its energy.

However, this is not what actually happens. All of the energy produced near the vibrating surface does not escape. Much of it simply sticks around the vibrating surface and never escapes. It simply adds to the mass of the vibrating surface. [Note that you noticed this when you dip a vibrating aluminium pot lid into water. The frequency drops because the vibrating mass has increased due to the water around the lid vibrating with the lid.] This is especially true at low frequency. If the wavelength of the sound is much larger than the dimension of the vibrating surface, most of the energy of vibration of the air near the vibrating surface does not radiate at all. I will call the fraction of the energy which actually makes it away from the surface and out into the air as sound the efficiency with which the sound escapes.

This efficiency depends on a number of factors. It depends on the exact shape of the vibrating surface. It depends on the surrounds of the vibrating surface (eg whether the speaker is mounted in a solid wall which extends as a flat wall far from the speaker, or if it is mounted in a box about the same size as the speaker.) It furthermore depends most crucially on the whether or not the sound can get to the listener only from one face of the vibrating object or from more than one. Let me first look at the case where the wavelength of the sound is much larger than the dimensions of the vibrating object. In the case where the sound can get out from only one face of the speaker, the efficiency factor is given roughly

as the square of the ratio of twice the size of the system divided by wavelength, or $\left(\frac{2D}{\lambda}\right)^2$, as long as the wavelength is much larger than the diameter of the vibrating system. If on the other hand the sound can get to the listener from both sides of the vibrating surface, the efficiency is now approximately given by $\left(\frac{2D}{\lambda}\right)^4$ for wavelengths much larger than the diameter. If one has two vibrating areas in which both sides of each diaphragm emit sound that can get to the listener and the two vibrate in opposite directions (eg, tuning fork) , then the sounds from the two almost cancel, and in this case the efficiency goes as $\left(\frac{2D}{\lambda}\right)^6$.

In all of the above cases on the other hand, for frequencies which are much higher than those for which the wavelength is about the same as the diameter of the object, (ie, the wavelengths are much smaller than the size of the object) all of the energy gets out and the efficiency is unity.

In the intermediate regime, the situation becomes complicated. However as a first approximation, we can simply take the efficiency as 1 for all frequencies such that $\lambda/2$, half the wavelength, is smaller than D the diameter, and as $\left(\frac{2D}{\lambda}\right)^2$ if the wavelength is larger than the diameter for the case of a simple one sided piston. For the case of a two sided piston, I will take the expression as 1 for $\lambda/2 < D$ and as $\left(\frac{2D}{\lambda}\right)^4$ for $\lambda > D$. For the case with two vibrating diaphragms, in which they vibrate in opposition to each other, I will take it as again 1 for $\lambda/2 < D$ and $\left(\frac{2D}{\lambda}\right)^6$ for $\lambda/2 > D$.

Note that these expressions are crude approximations, and the actual frequency of transition can vary depending on the exact shape of the vibrating body, its enclosure, etc..

In the case of the diaphragm for which one can hear the sound from both sides, the answer depends not only on the diameter of the vibrating diaphragm, but also on how far the sound has to travel to get to the listener from the back of the diaphragm. Similarly in the case of two out of phase diaphragms, the distance between the diaphragms is also important. A better approximation would be to write the expression in this third case as

$$\left(\frac{2D}{\lambda}\right)^2 \left(\frac{2W}{\lambda}\right)^2 \left(\frac{2L}{\lambda}\right)^2$$

, where W is the width of the barrier in which the speaker is mounted (ie the distance the

sound has to go to get around from the back to the front where the listener is, and L is the distance between the two radiating "diaphragms". However even this expression is a rough estimate of the efficiency. We however are not carrying out detailed calculations, but are simply trying to get a feeling for the effects. Thus, for the purposes of this course I will always use the above crude approximations.

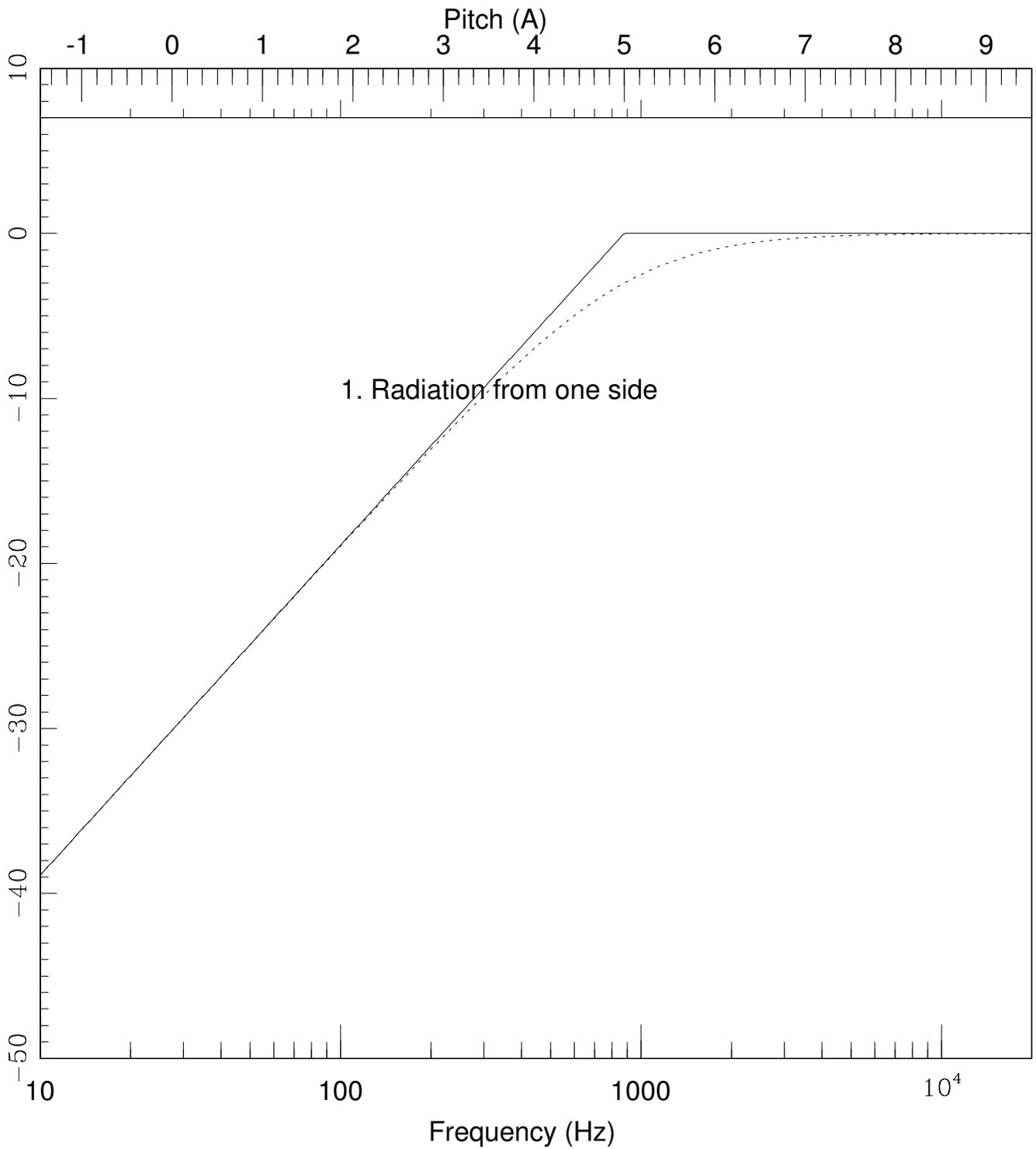
In order to present this data in a more graphical instead of an algebraic fashion, let me graph the efficiency factor. I will choose to graph it using the dB scale to represent the ratio of energies (energy actually emitted over energy expected to be emitted based on velocity near the vibrating body), and will use pitch to represent the frequencies.

Remember that each 10 dB change (on the 'y' axis) represents a factor of 10 change in the efficiency. On the 'x' axis, each change in pitch by one octave represents a change by a factor of 2 in frequency, and a also a factor of two change in wavelength. (If the frequency goes up by a factor of 2, the wavelength shortens by a factor of 2). On this scale, we note that the function $\left(\frac{D}{\lambda}\right)^2$ is such that as the wavelength increases by a factor of 2 (and the frequency decreases by an octave), the efficiency goes down by a factor of $2^2 = 4$. Looking on the relative dB scale, we note that a factor of 4 corresponds to approximately 6 dB. Thus each time the frequency changes by an octave, the efficiency changes by 6 dB. This produces a graph in which the efficiency rises by 6dB for each octave rise in frequency, as long as the frequency is low enough.

For high frequencies, the efficiency is unity. Since a ratio of unity corresponds to 0 dB, the plot of the efficiency on this graph can be obtained as follows. Calculate the frequency at which half the wavelength equals the diameter. Call this the "knee" frequency. For frequencies larger than this knee frequency, plot a horizontal line along the 0 dB line. For frequencies less than this knee frequency, plot a straight line which falls 6dB for every octave and goes to 0 dB at the knee frequency. Use this as the approximation to the efficiency for the sound source with diameter corresponding to half the wavelength at the knee frequency.

I have done this for a particular example of a sound source a plane diaphragm of diameter 19.3 cm. First we need to calculate the knee frequency. This corresponds

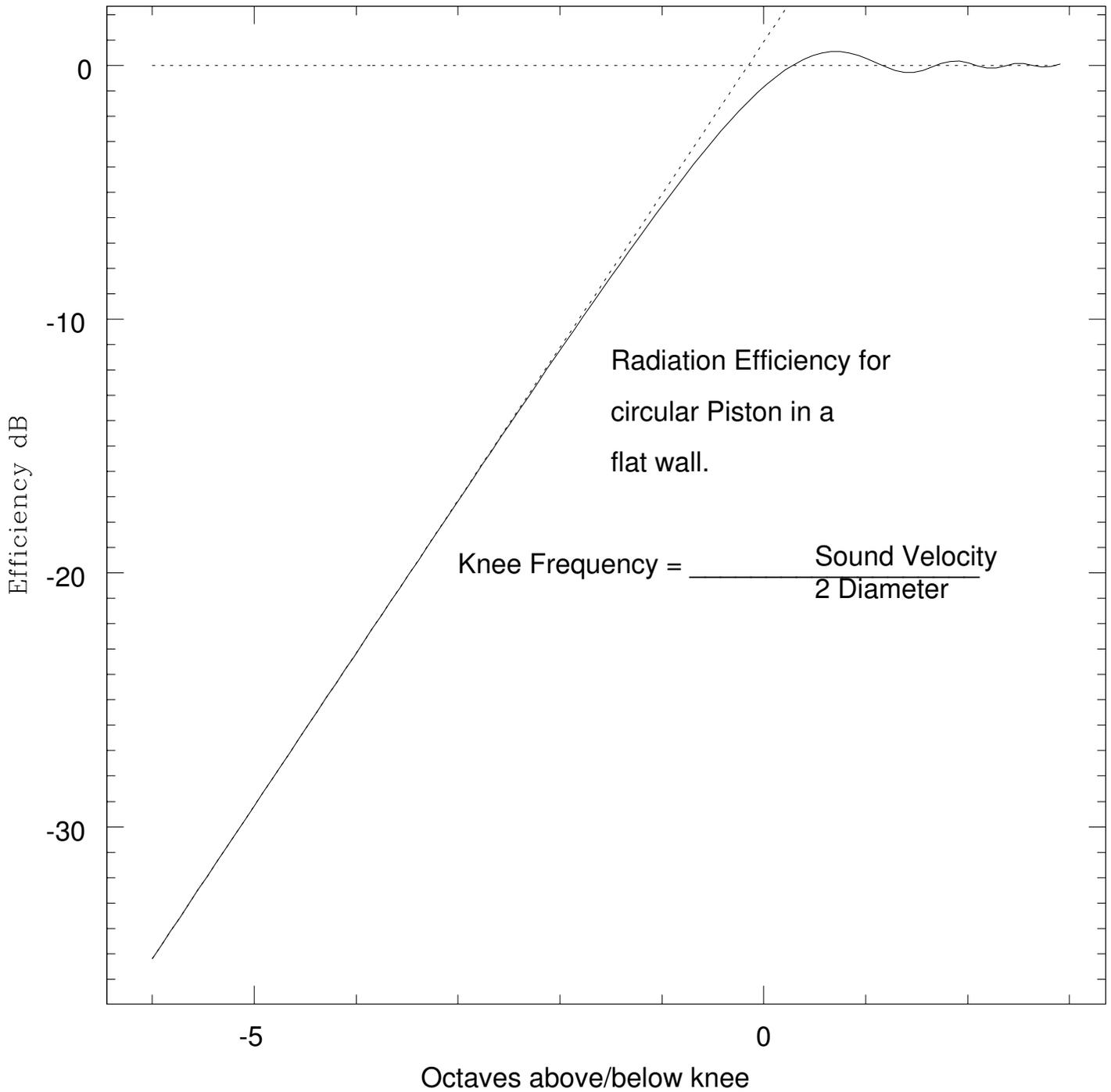
to a wavelength equal to twice the diameter, or 38.7cm. This wavelength corresponding to the knee frequency of is $\frac{340m/sec}{.192m} = 880Hz$. For frequencies higher than 880 Hz (ie, A880), the efficiency line is a horizontal line at 0dB. For lower frequencies, the line must fall by 6dB per octave. We therefor go down one octave from 880Hz, to 440Hz (or the 3rd A along the pitch axis). Plot a point at this frequency and at -6 dB. Draw a straight line from the 880Hz-0dB point through this 440Hz -6dB point. We thus get the plot in figure 1 for the efficiency for this particular vibrating diaphragm.



If we now want to discover with what efficiency this diaphragm will radiate at some frequency, say 200Hz, we simply read off the graph what the efficiency corresponds to at 200Hz. In this case it is approximately -12.5dB. Only a fraction of about 1/18 th

($12.5\text{dB}=10\text{dB}+2.5\text{dB}$ which corresponds roughly to a factor of 10×1.8) of the sound energy of vibration of the air at the diaphragm will actually escape as sound.

It is of course clear that this graph is an approximation. No physical function ever has sharp corners as this one does at the knee frequency. The true efficiency curve would be a smooth curve, with no sharp corners. The dotted line represents one possible actual curve. For a speaker in an infinite flat wall, the curve in addition has wiggles around the knee frequency. In the next figure 1a is plotted the actual efficiency as a function of frequency for a flat circular piston in an infinite flat wall. Note that the actual knee frequency is in fact slightly lower than the approximation we have made. The location of the actual knee depends on a large number of factors, most important being the shape of the enclosure the sound source is in. However, we will not worry about this in this course.

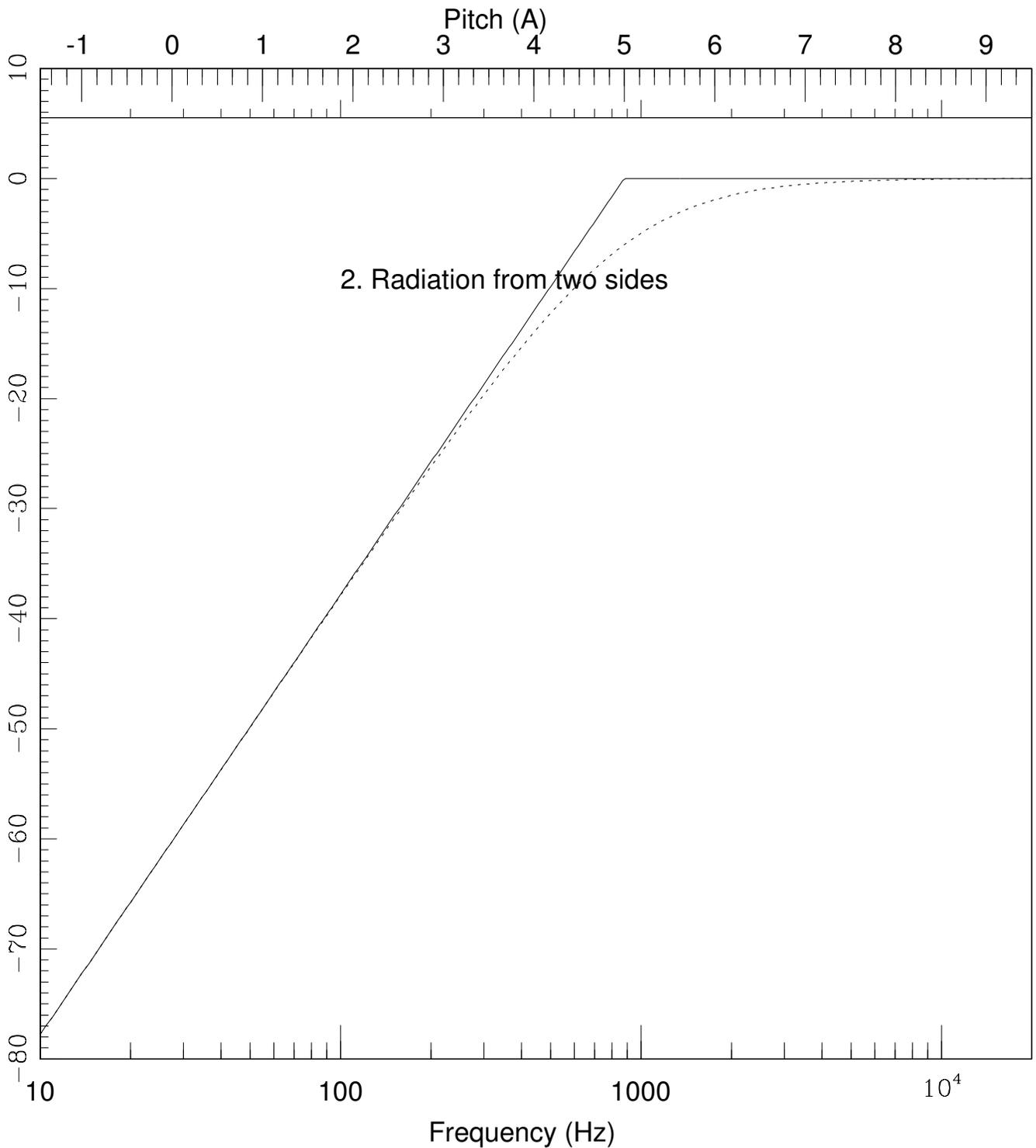


Note that there are also wiggles in the efficiency for frequencies above the knee. On a dB scale these wiggles are audibly negligible, since they are less than 1dB in amplitude. These wiggles come about because of interference from the various parts of the speaker in

directions off the straight ahead direction.

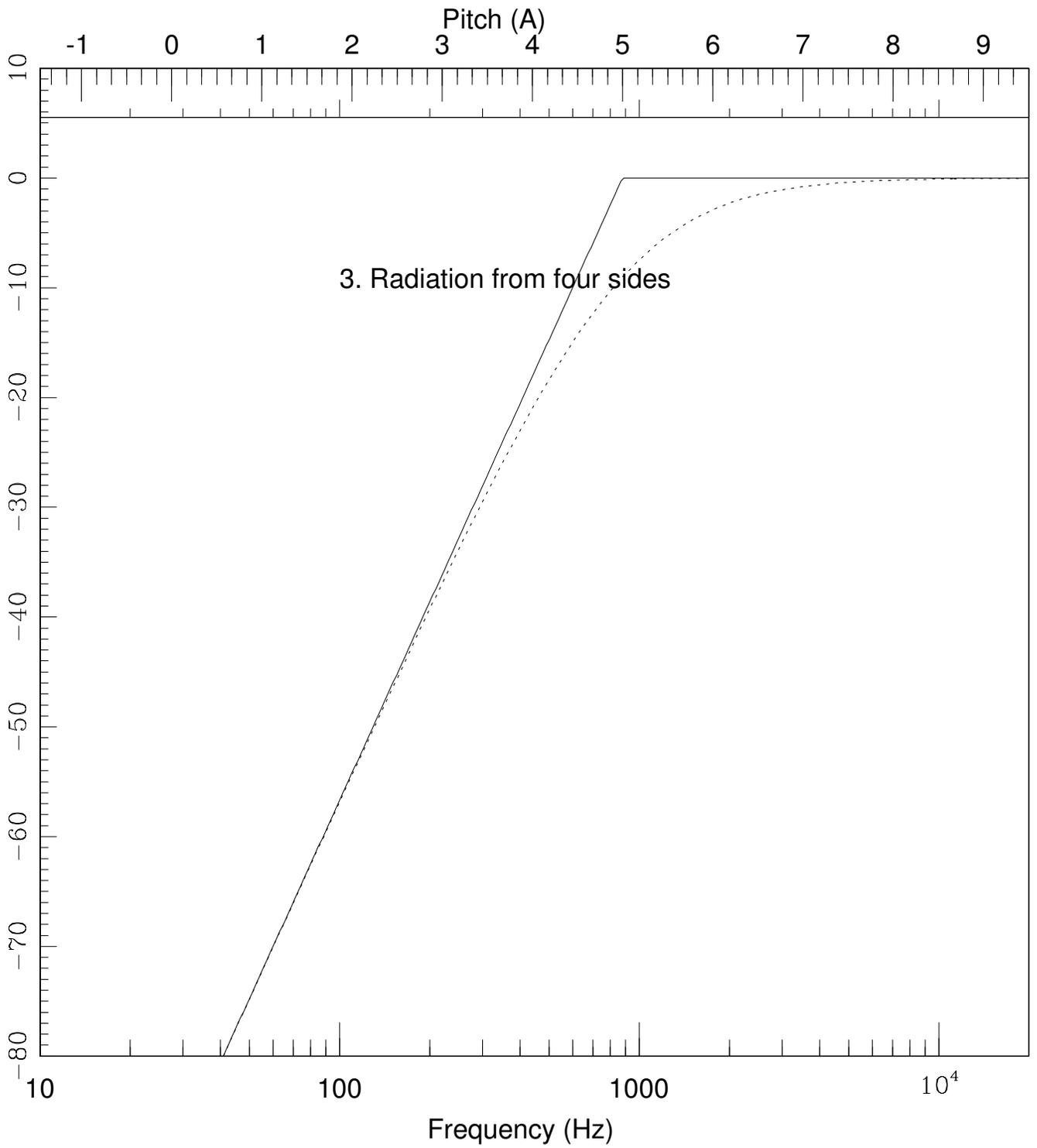
Note that sharp edges on a speaker also tend to produce wiggles in the response at frequencies where the size of the box is roughly half a wavelength in size.

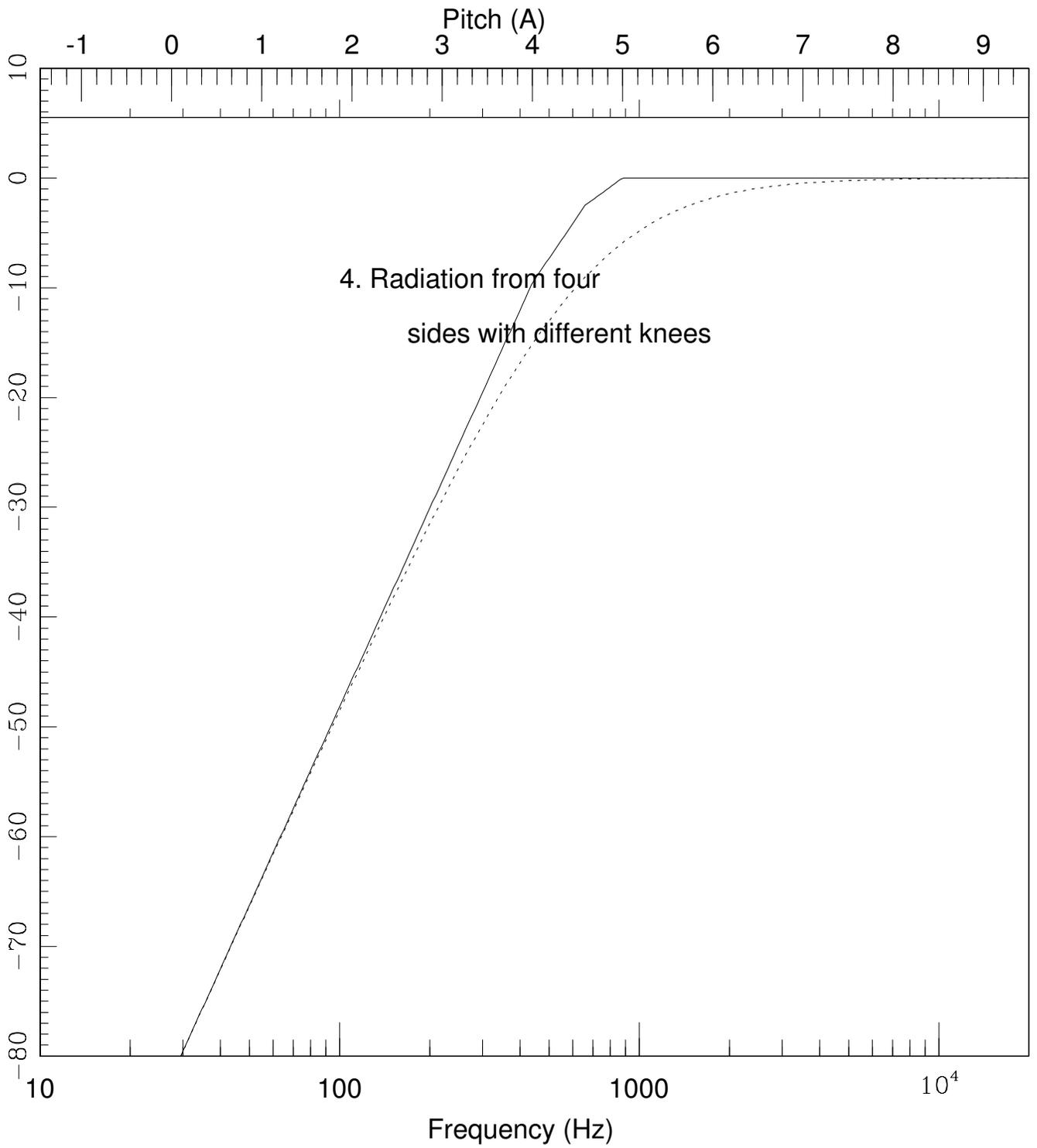
If both sides of the speaker are open to the air, so that the sound from the back can get to the listener, as well as sound from the front, then instead of a 6dB per octave curve for frequencies below the "knee" frequency, the efficiency falls at 12dB/octave instead. Ie, since the efficiency goes as $\left(\frac{D}{\lambda}\right)^4$, if λ increases by a factor of 2, the efficiency drops by a factor of $2^4 = 16$. But $16 = 1.6 \times 10$ which is 2 dB (for the factor of 1/6) plus 10dB (for the factor of 10) to give 12dB. Ie, the curve should be drawn so that it rises by 12 dB every time the pitch changes by an octave, as in figure 2.



If we have a system like a tuning fork, where there are two vibrating elements both of which vibrate in opposite directions to each other, then the curve slopes as 18 dB per octave below the knee frequency. ($2^6 = 64 = 6.4 \times 10 \rightarrow 8dB + 10dB = 18dB$) This is plotted in

figure 3. Note that in order to get most of the curve onto the plot, I have vastly expanded the range of the dB axis. Instead of going from -30dB to 10dB, it here goes from -120 dB to 10 dB. Of course again in this case the true curve will be smoother than this one with its drastic kink, and there will be oscillations in the curve around the knee frequency. But again these are matters for more detailed study, not for this course where we are trying to simply get a feel for what is happening. (If you want more details, the course which meets in our lecture room immediately before ours is one in which the details of acoustics are calculated mathematically.) Even without straight line approximations, we could improve things by calculating three "knee" frequencies- one for the size of the "piston" (D), one for the distance around from the back to the front of the piston (W), and one for the separation of the two radiating surfaces (L) at each "knee" frequency, the line changes in its slope, from 18dB per octave, to 12dB per octave, to 6dB per octave, to the high frequency (small wavelength) region above all the knees of 0dB. (see figure 4). Again it just isn't worth it.



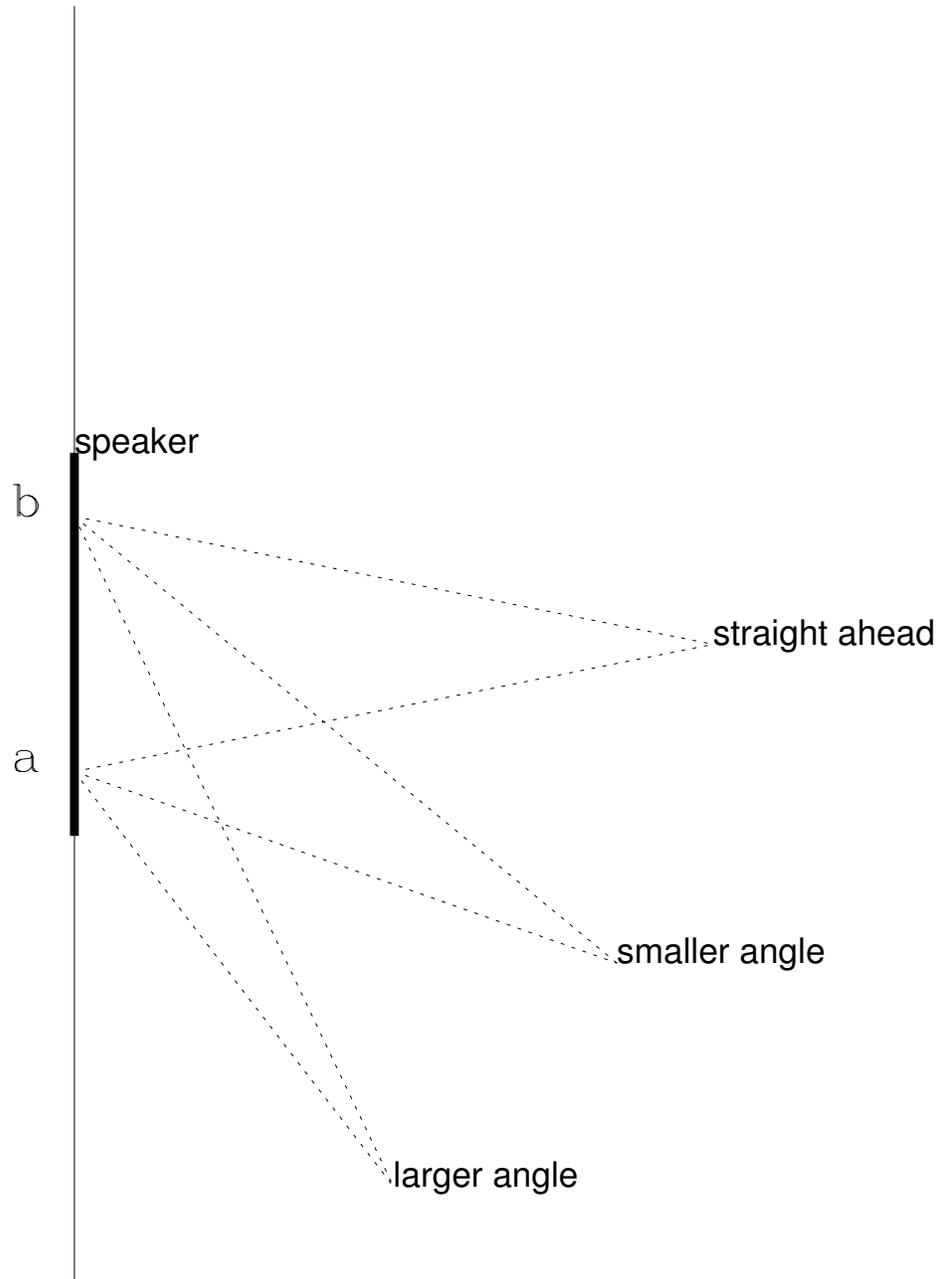


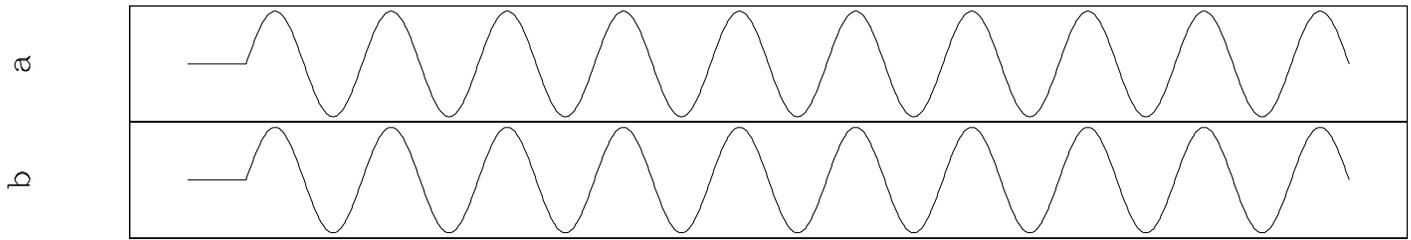
II. INTERFERENCE

What causes these effects? In particular, why if one can hear both sides of the diaphragm is the amount of sound radiated at low frequencies so much less than if you can hear only one side of the piston? The phenomenon is one called interference. Let us examine this situation in which one has a vibrating diaphragm and for which both sides of the diaphragm can be heard. For frequencies much less than the "knee" frequency, each side of the diaphragm produces sound. However the sound from the back of the piston is 180° out of phase with the sound produced by the front. Ie, when the front produces a disturbance with the velocity of the air in one direction, the back produces one with the velocity and pressure in exactly the opposite direction. If they were immediately combined, they would completely cancel and produce no sound whatsoever. However, the sound from the back of the diaphragm has to travel a slightly greater distance than does the sound from the front if the listener is in front of the diaphragm. As a result when the sounds from the two sides reach the ear, they are not exactly opposite in pressure and velocity. When the sound from the front reaches the ear with a maximum velocity in its oscillation, the sound that reaches the ear from the back must have left the diaphragm slightly earlier than that from the front, in order to make up for the extra time it took to travel to the ear. As a result the sound front the back is not exactly at its minimum (most negative) velocity, and that sound from the back does not exactly cancel that from the front. The phase difference is not exactly 180° , and the two waves do not exactly cancel. The longer the wavelength (ie the lower the frequency) the less of a difference in phase this small difference in travel time makes, and the more nearly the waves cancel. This near cancellation of the waves from the different parts of the diaphragm is called interference. The sounds from the two sides of the diaphragm interfere with each other, and produce far less sound that one would otherwise expect.

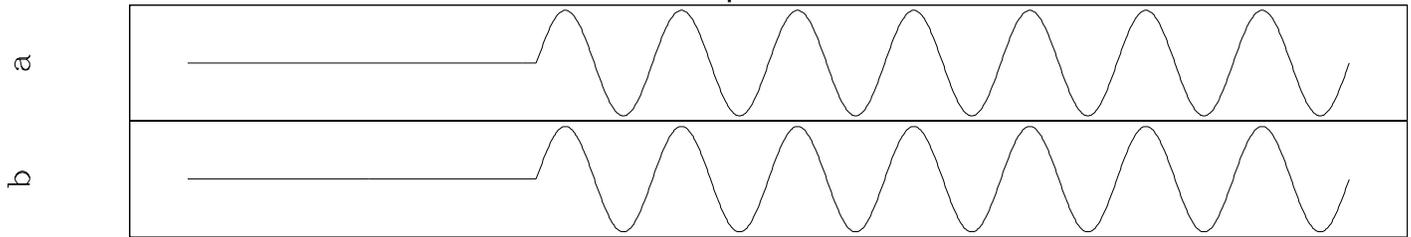
Simialry, the sound from various parts of the speaker can interfere with each other. In figure 5 we have a speaker in the wall (so sound only comes from one side) and an ear a distance away from the speaker at various angles to the speaker. We want to look at the

sound getting to the ear from the two points a and b on the speaker. Sound takes time to travel from the speaker to the ear. If the ear is straight ahead, the sound from both points has the same distance to travel.(see figure 6) If the two points on the speaker are vibrating in phase, the sound that gets to the ear will be in phase, and the two sound waves from these two parts of the speaker will add together. At point at a smaller angle however the distance from b is larger than from a. The sound getting to the ear from b will be delayed. In this example I am assuming that the delay is about $1/4$ of a period (ie, the difference in distances is about $1/4$ wavelength). The two waves from teh two points do not completely add together. and the sound will be less than straight ahead. At the larger angle, the distance from b is even larger than from a. By assumption it is now $1/2$ a period difference in time of arrival. Now the two sounds are completely out of phase and cancel at the ear.

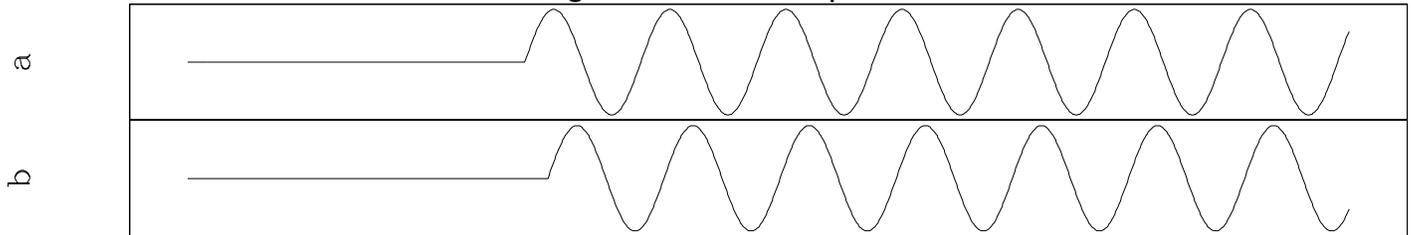




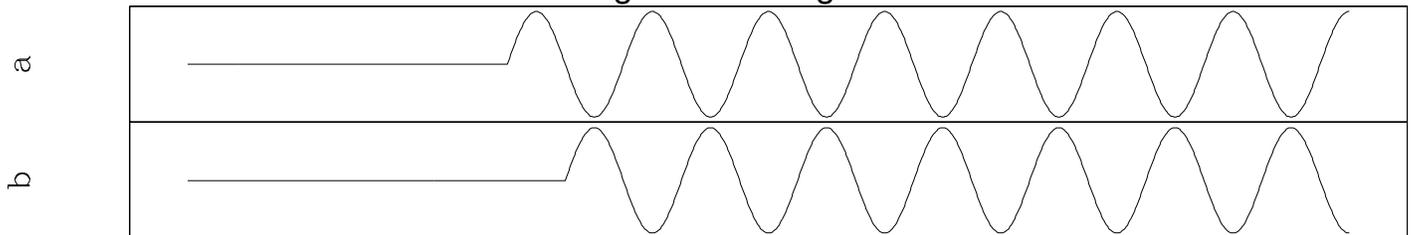
at speaker



straight ahead from speaker



at smaller angle from straight ahead



at larger angle from straight ahead.

Clearly one must go through this procedure for each part of the speaker to find out how much sound actually gets to the ear, and how much the various parts of the speaker cancel each other out. Clearly, if the speaker is larger in diameter than half a wavelength, then the

sound delay from any part will be less than half a period, and the sound does not completely cancel from any two parts of the speaker.

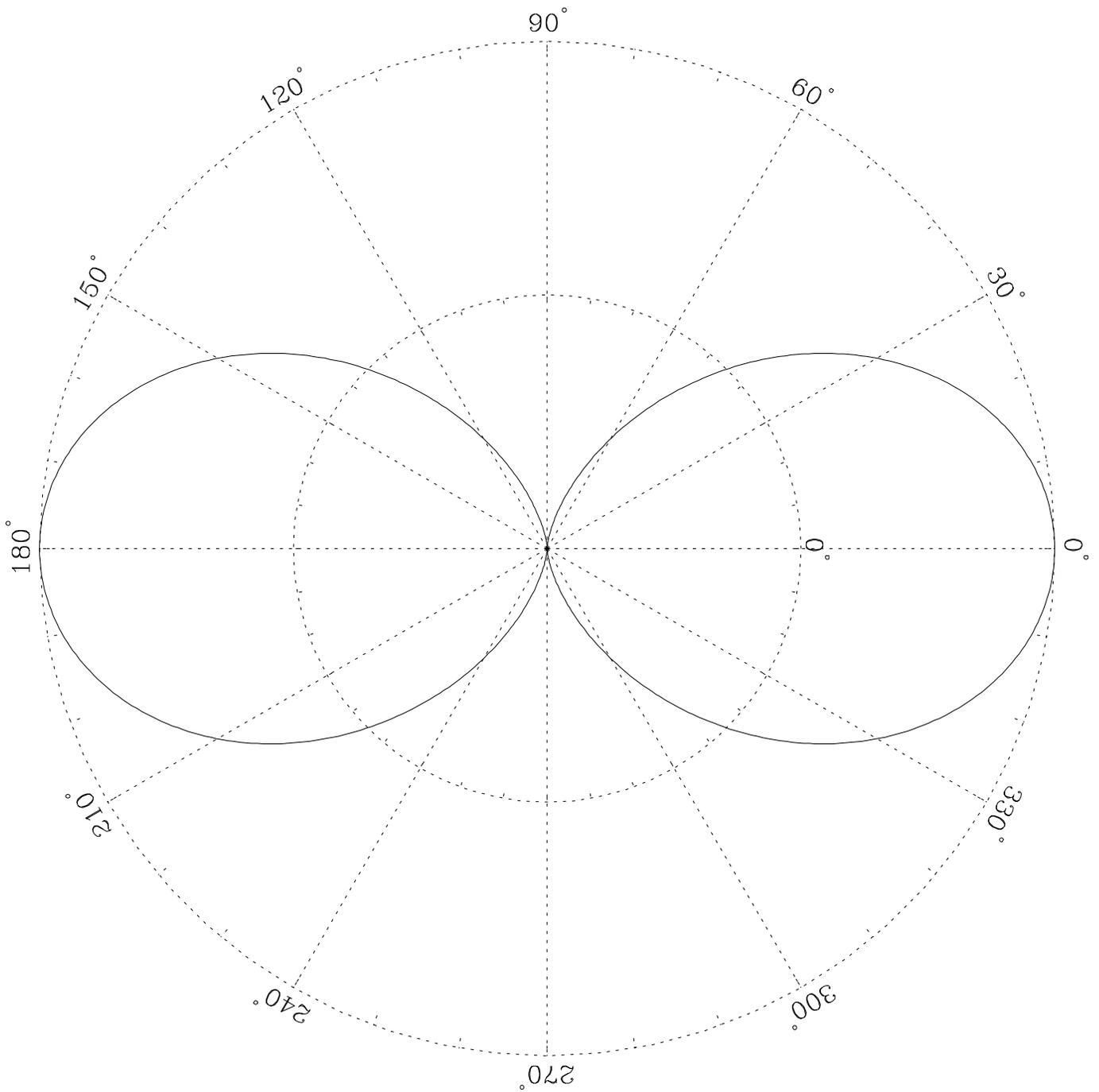
III. DIRECTIONALITY

One of the key idea that can be picked up from the preceding paragraph is what sound someone would hear it they were placed away from a vibrating diaphragm but were located in the same plane as the diaphragm. In this case the distance that the sound has to travel to them from the two sides of the diaphragm are exactly the same. Since the two sides produce sound of exactly 180° out of phase with each other, and the time taken to get to the ear from the two sides is exactly the same, the sounds will cancel at the ear. Ie, there will be no sound emitted in a direction parallel to the diaphragm. However if the observer sits either behind or in front of the diaphragm, sound will be heard. Ie, the sound emitted from a vibrating diaphragm, where both sides radiate freely into the air has directional properties due to interference of the sound coming from the various parts of the oscillating source.

The same is true for the sound coming from a single side of the diaphragm. If the wavelength of sound is much smaller than the diameter of the oscillating diaphragm, then even the sounds emitted by different parts of the diaphragm can interfere with each other. Since the distance sound travels in one period is by definition one wavelength, if the wavelength of the sound is less than the diameter of the diaphragm, then the time at which the sound gets to a listener listening off axis of the diaphragm will differ, and can differ by times which are equal to or even much greater than one period. This means that the sound which gets to the ear from the different parts of the diaphragm will have very different phase relations. Some will cancel, some will add and one has to do detailed calculations. The results are that if the wavelength is of the order of or much less than the diameter of the source, then the sound coming off is highly directional. Almost all of the sound comes off in the straight forward direction. In fact roughly, the angle into which most of the sound is radiated is of the order of $50^\circ \frac{\lambda}{D}$. The larger the diaphragm with respect to the wavelength, the narrow

this angle is, and the more directional the sound is that comes off the diaphragm. This can of course be useful at times, but demonstrates that if one wants the sound to only go into a certain direction one needs a very large radiating size.

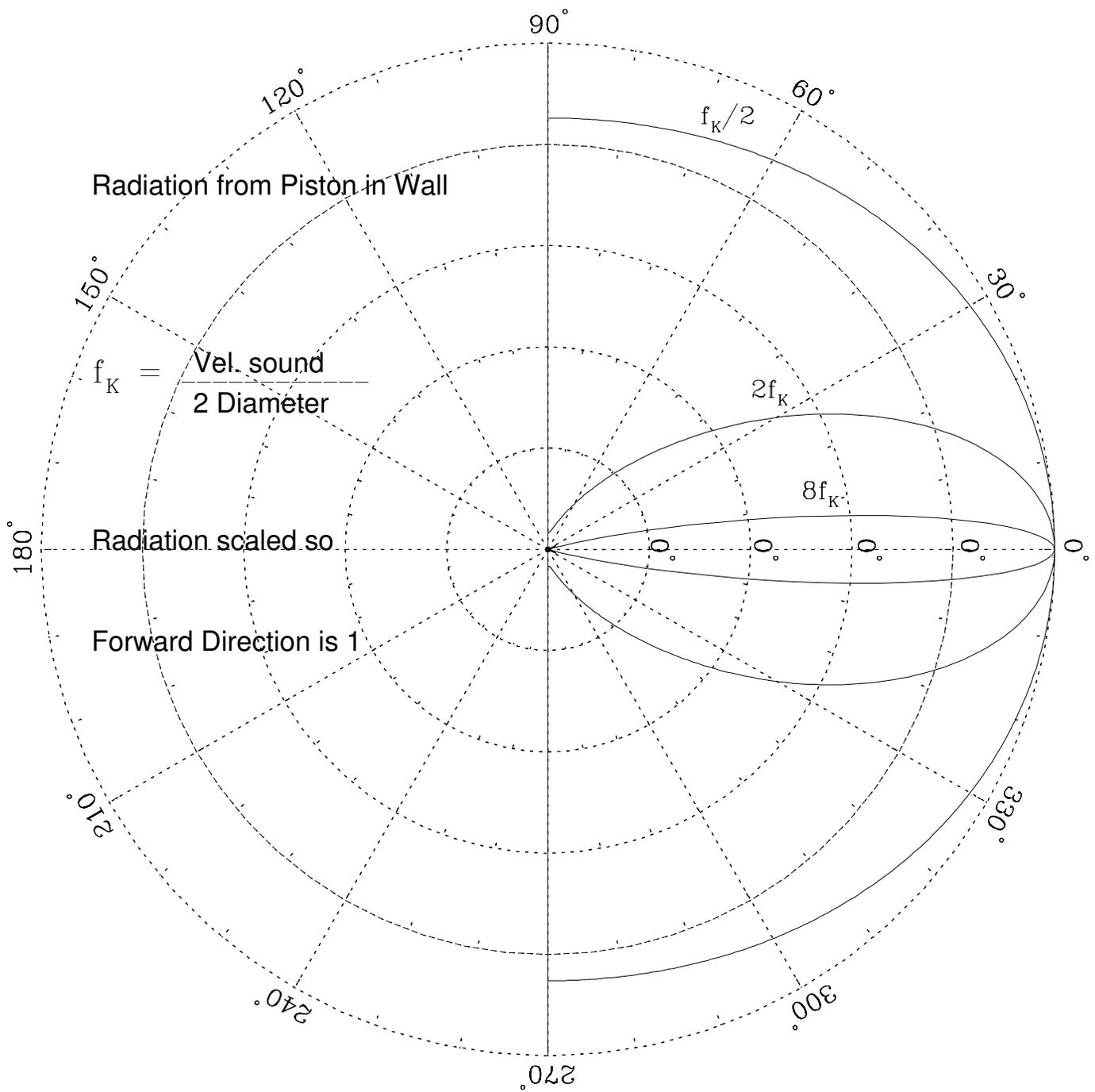
In figure 7 I have plotted the "dipole" response pattern of a system which radiates from two sides, and at a frequency much lower than the knee frequency. This plot is a polar plot. It plots the relative intensity of the sound emitted in various directions. Note that the sound is a maximum in the zero degree and 180 degree directions, and goes to zero, as argued, in the directions perpendicular to the motion of the speaker.



5. Radiation direction for dipole radiator.

The amount of energy going into certain directions is usually graphed on a type of graph called a polar diagram. This is not a graph with axes in the usual sense. Instead, one is trying to represent how much sound is radiated into a certain direction. To do this, one

chooses an origin (some point) and from that origin draws straight lines going outwards from that point in the various directions one is interested in. Then along the line going in a particular direction of interest, one measure a distance along that line from the central point corresponding to the magnitude of the energy one wishes to represent on the graph, and puts a point there. Doing this for all of the directions, and then joining up the points smoothly, one gets the polar diagram. Figure 8 is one such example. These graphs are almost always relative graphs. Ie, one does not plot the absolute energy going in any particular direction but picks some direction (eg straight ahead) as the fiducial direction, and calls the amount radiated in that direction 1. Ie all of the energies are measured as ratios with the energy going straight ahead in the denominator.



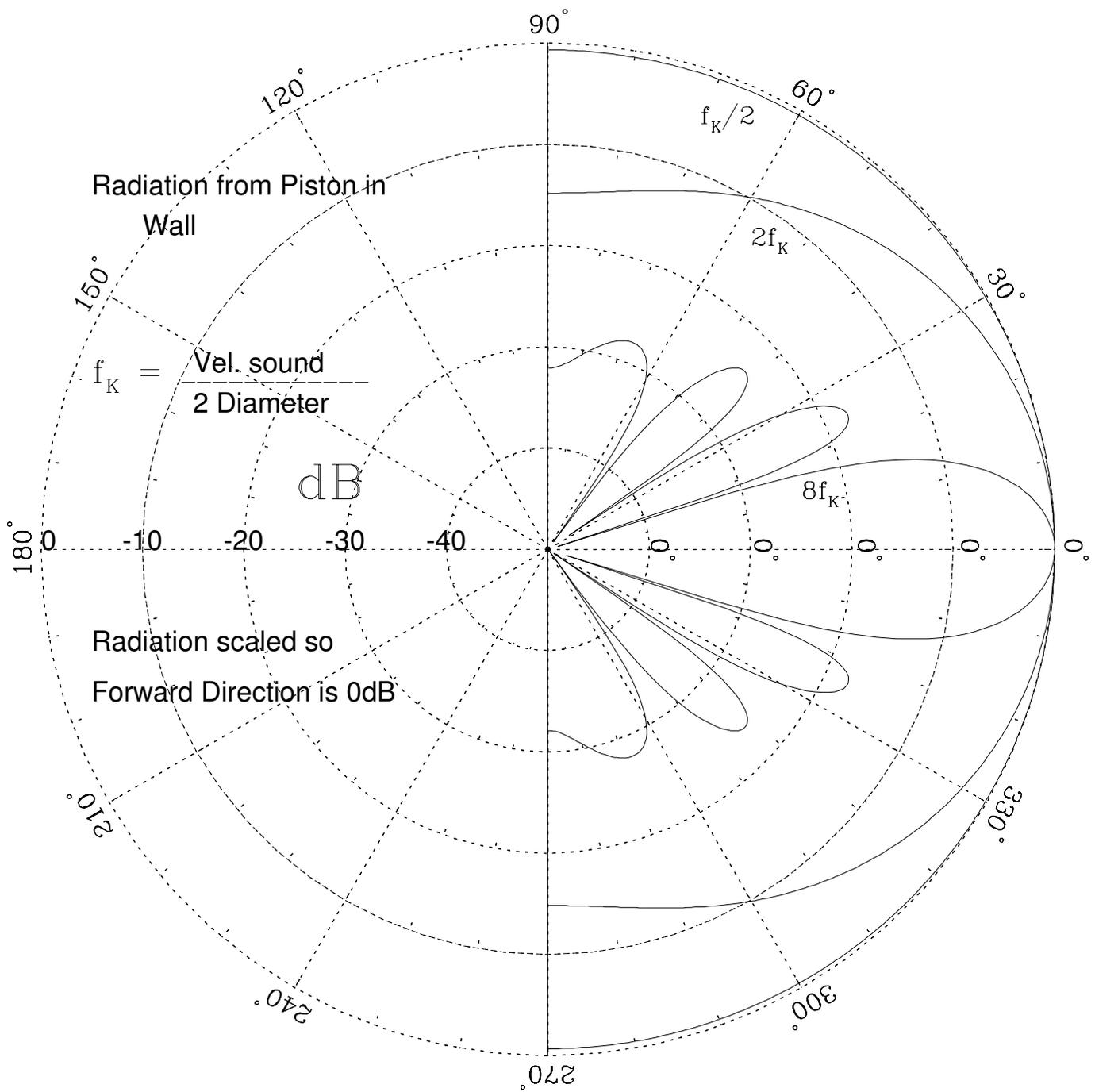
Radiation Distributions

So let us look at figure 8. In the straight ahead direction (0°), the distance along the line going straight ahead is of magnitude 1. Along the 45° direction reading along the radius there, the magnitude is .5, which means only half as much energy gets radiated in the 45°

direction as in the forward direction. In the 90° direction, the magnitude is zero, meaning that no radiation is emitted in that direction. In the 180° direction, the magnitude is again 1, meaning that just as much radiation is emitted in the backwards direction as in the forwards, etc. Note that this graph is in fact the graph of the radiation direction for a diaphragm in which both sides are radiating at frequencies much less than the "knee" frequency (wave length much larger than the diameter of the radiator). This pattern of radiation is known as the "dipole" pattern. It is also the pattern of radiation from a violin at frequencies above about A440 to about 1kHz.

We can now look at the pattern of radiation from a single diaphragm mounted in a wall, say. Obviously in this case the energy is only radiated in the forward direction, since the observer cannot be located inside the wall. At low frequencies, the radiation is emitted almost equally in all directions. As the frequency rises the direction of the radiation emitted becomes more and more focused. In Figure 6 I have plotted the directionality of the radiation for three frequencies– half the knee frequency in which case the radiation is essentially isotropic, twice the knee frequency, in which case the radiation has begun to be beamed in the forward direction, and 8 times the knee frequency, in which case the radiation is emitted in a narrow cone straight ahead.

In Figure 9 I have plotted exactly the same radiation from a simple piston in a wall, but in this case, I have plotted the intensity in dB rather than in the relative intensity. Here it is easy to see that the radiation pattern becomes "lobed" at high frequencies, where directions of no radiation alternate with directions of some (although by far the most goes into the lobe pointing straight ahead). These lobes and zeros are caused by the interference of the radiation from the various parts of the diaphragm interfering with each other, and in some directions it entirely cancels out, while in other directions it partially cancels, but not entirely. Note that even the largest lobe is about 18dB below the intensity of the straight ahead radiation, and thus is scarcely noticeable in the polar intensity plot.



Radiation Distributions (dB)

One point is that the graphs have all been plotted taking the efficiency of the straight ahead radiation to be unity. Ie, the intensities plotted have been relative intensities. However in actual fact, the intensity straight ahead rises by a factor of 4 per octave for all frequencies.

Ie, given that the piston vibrates with the same velocity, the intensity straight ahead would be 16 times higher for the $2f_k$ than for the $f_k/2$, and another 16 times more intense for the $8f_k$. Ie, a vibrating piston becomes louder and louder right on axis the higher the frequency, but falls off more and more rapidly as one goes off axis.

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